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borehole is kept full of water or bentonite mud and the tendency to bottom heave is drastically reduced; block samples can be obtained at much greater depths than in an open trench. Experience at different locations in Quebec has demonstrated the ability of this type of apparatus to obtain block samples under various field conditions.

# Acknowledgments

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corrections made during the development of the sampler.

Béland, J. 1955. Nicolet landslide. Proceedings of the Geological Association of Canada, 8(1), pp. 143-156.

Berre, T., Schjetne, K., and Sollie, S. 1969. Sampling disturbance of soft marine clays. Specialty Session I, 7th International Conference on Soil Mechanics and Foundation Engineering, Mexico, pp. 11-14.

BOZOZUK, M. 1970. Effect of sampling, size and storage on test results for marine clay. American Society for Testing and Materials, Special Technical Publication 483, pp.

EDEN, W. J. 1970. Sample trials in overconsolidated sensitive clay. American Society for Testing and Materials, Special Technical Publication 483, pp. 132-142.

LA ROCHELLE, P., and LEFEBVRE, G. 1970. Sampling disturbance in Champlain clays. American Society for Testing and Materials, Special Technical Publication 483, pp. 143-163.

RAYMOND, G. P., TOWNSEND, D. L., and LOJKASEK, M. J. 1971. The effect of sampling on the undrained soil properties of a Leda soil. Canadian Geotechnical Journal, 8, pp. 546-557.

# The bellow-hose settlement gauge

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Bellow-hose settlement gauges were used to measure vertical soil heave during the installation of concrete piles in sensitive marine clay. The equipment is described and the sources of error are discussed.

Des tassomètres à tube compressible ont été utilisés pour mesurer les soulèvements verticaux du sol lors de l'installation de pieux de béton dans une argile marine sensible. On décrit l'équipement et on discute les causes d'erreurs. [Traduit par la revue]

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## Introduction

Several thousand end-bearing concrete piles, required for the expansion of a large industrial plant in eastern Canada, were to be driven through sensitive marine clay. To study how adjacent foundations are affected by driving a large group of piles, a research program was initiated to measure the soil and pile

movements on a selected group of 116 piles (Bozozuk et al. 1978). This note describes the bellow-hose settlement gauge used to measure the vertical soil movements as the pile driving program was carried out.

## **Bellow-hose Gauge**

The bellow-hose settlement gauge is similar to that developed by Wager (1973). It consists of a spirally reinforced axially flexible polyethylene tube 40 mm

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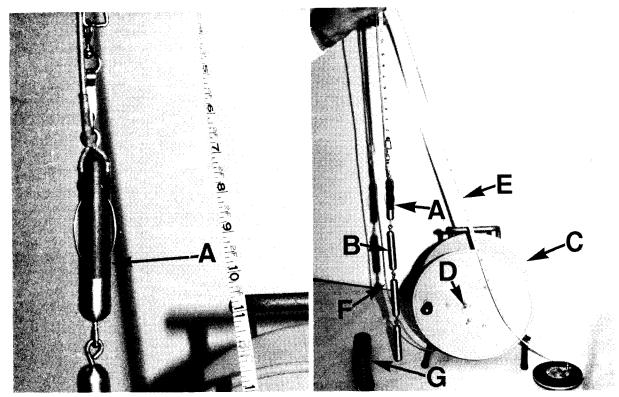


Fig. 1. Components of bellow-hose settlement gauge: A = electric probe with flexible spring contacts;  $B = \text{gauge weights } (3 \times 500 \, \text{g})$ ; C = reel; D = voltmeter; E = measuring tape (in inches); F = electric connecting cable; and G = sample of axially compressible bellow-hose. (Photos: B. H. Fellenius, Terratech Ltd., Montreal.)

in diameter, equipped with 50 mm long, 25 mm inside diameter metal rings mounted at predetermined locations to serve as measuring points.

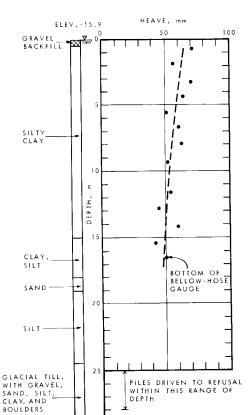
To install the gauge, a 60 mm diameter casing is first placed to the desired depth. In soft soils, the bottom of the casing is plugged and pushed down; in stiff soils, the casing is drilled and washed, care being taken that the surrounding soil is not overwashed, which would create voids around and underneath it. The bellow-hose is filled with water, a 10 mm grouting hose is loosely attached to the bottom end, and both are lowered into the casing. A 20 mm diameter iron pipe is then inserted to the full length of the bellow-hose and secured at the top to stabilize and support the installation during grouting.

A bentonite-cement grout consisting of one part Portland cement and four parts bentonite at a water content of 350% is pumped through the grout hose to fill the void between the bellow-hose and the soil. The casing and the grout hose are withdrawn simultaneously and gradually, taking care to ensure that the grout level is always above the bottom of the casing and the tip of the grout hose. Finally, the top of the bellow-hose is secured to a 1.8 m length of

protective casing and grouted to the soil at the ground surface; then the 20 mm diameter iron pipe is withdrawn.

The elevations of the measuring rings are determined by means of an electric probe attached to a measuring tape (Fig. 1). The probe consists of a 100 mm long, 20 mm outside diameter plastic body connected to three spool-shaped steel 500 g weights that hang from it. Three equally spaced arch-shaped steel springs 30 mm long protrude about 5 mm from the side of the probe. The steel springs are electrically insulated from each other, but two of them are connected to a cable leading from the probe to a voltmeter. When the probe contacts the metal rings, the electric circuit is closed, activating the voltmeter. The cables and the measuring tape are coiled together on a drum from which they are fed into the bellow-hose. Measurements can be made by one man. The measuring time for a gauge 18 m deep with contact rings installed at 2 m intervals of depth is about 20 min.

Measurements are performed by first lowering the probe to the bottom of the hose and then lifting it up to contact each ring in turn, and recording the distance to the top of the settlement gauge. The elevaNOTES 235



BELLOW-HOSE NO. 45

Fig. 2. Variation of measured soil heave with depth within group of driven piles.

tions of the rings are obtained from the elevation of the top of the gauge, which was determined from level surveys.

A number of factors affect the accuracy of the measurements. The direct reading error has been established by repeated measurements to be a maximum of  $\pm 2$  mm. In connection with pile driving, however, horizontal soil movements occurred that caused the metal rings to tilt. The three steel springs eliminated most of this error, but additional inaccuracy appeared. Including the effect of weather, time, etc., on human performance, the actual combined error was about  $\pm 5$  mm. When errors inherent in level surveying to the gauges were added, the possible total error increased to about  $\pm 8$  mm.

Survey errors can, however, be reduced either by anchoring the bottom of the bellow-hose in firm soil not subject to soil movements, or by installing a deep bench mark directly outside the bellow-hose gauge.

Figure 2 shows the variation of measured heave to a depth of 16.5 m after driving a group of 116 concrete piles around an installation in marine clay. The deviation of the measured values from the average line are within  $\pm 8$  mm, the stated accuracy of the gauge.

### **Summary and Conclusions**

The bellow-hose settlement gauge proved to be a useful field instrument for measuring the variation of soil heave with depth at a given location. It has an accuracy of  $\pm 2$  mm if installed in a soil not subjected to horizontal soil movements and with its lower end seated in a firm soil formation. In the present case, however, the soil was subjected to horizontal movements that caused the measuring rings to tilt, and the position of the bottom of the bellow-hose was affected by the pile driving. Level surveys were required to establish a datum elevation for each set of measurements. The resultant combined error increased to  $\pm 8$  mm.

The advantage of this equipment is that vertical soil movements can be measured at numerous predetermined elevations quickly and easily at one installation.

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BOZOZUK, M., FELLENIUS, B. H., and SAMSON, L. 1978. Soil disturbance from pile driving in sensitive clay. Canadian Geotechnical Journal, 15(3), pp. 346-361.

WAGER, O. 1973. Bälgsättningsmätare för mätning av vertikalrörelser i jord. Lecture at the Nordic Geotechnical Meeting, Trondheim in The Norwegian Geotechnical Society Report, Oslo, Norway, pp. 95–98. (In Swedish.)